Coupled BEM–FEM for the convected Helmholtz equation with non-uniform flow in a bounded domain

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\textbf{Abstract}

We consider the convected Helmholtz equation modeling linear acoustic propagation at a fixed frequency in a subsonic flow around a scattering object. The flow is supposed to be uniform in the exterior domain far from the object, and potential in the interior domain close to the object. Our key idea is the reformulation of the original problem using the Prandtl–Glauber transformation on the whole flow domain, yielding (i) the classical Helmholtz equation in the exterior domain and (ii) an anisotropic diffusive PDE with skew-symmetric first-order perturbation in the interior domain such that its transmission condition at the coupling boundary naturally fits the Neumann condition from the classical Helmholtz equation. Then, efficient off-the-shelf tools can be used to perform the BEM–FEM coupling, leading to two novel variational formulations for the convected Helmholtz equation. The first formulation involves one surface unknown and can be affected by resonant frequencies, while the second formulation avoids resonant frequencies and involves two surface unknowns. Numerical simulations are presented to compare the two formulations.

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1. Introduction

The scope of the present work is the computation of linear acoustic wave propagation at a fixed frequency in the presence of a flow. When the flow is at rest, the simplest model is the classical Helmholtz equation for the acoustic potential. This equation can be reduced to finding unknown functions defined on the surface of the scattering object and solving integral equations which can be effectively approximated by the Boundary Element Method (BEM) \cite{41}. When the medium of propagation is non-uniform, a volumic resolution has to be considered using, e.g., a Finite Element Method (FEM). If such non-uniformities occur only in a given bounded domain, it is possible to benefit from the advantages of both a volumic resolution and an integral equation formulation. Coupling BEM and FEM at the boundary of the given bounded domain allows this. Coupled BEM–FEM can be traced back to McDonald and Wexler \cite{34}, Zienkiewicz, Kelly and Bettess \cite{45}, Johnson and Nédélec \cite{26} and Jin and Liepa \cite{25}. Over the last decade, such methods have been investigated, among others, for electromagnetic scattering \cite{21, 29, 30}, elasticity \cite{11}, and fluid–structure \cite{13} or solid–solid interactions \cite{33, 44}. Coupled BEM–FEM for the classical Helmholtz equation can present resonant frequencies, leading to infinitely many solutions. All these solutions deliver the same acoustic potential in the exterior domain, but the numerical procedure becomes ill-conditioned. This problem has been solved in \cite{8, 22}, where a stabilization of the coupling, based on combined field integral equations (CFIE), has been proposed by introducing an additional unknown at the coupling surface.

When the medium of propagation is not at rest, the simplest governing equation is the convected Helmholtz equation resulting from the linearized harmonic Euler equations. Nonlinear interaction between acoustics and fluid mechanics is not
considered herein; we refer to the early work of Lighthill for aerodynamically generated acoustic sources [31,32], to [20] for a review on nonlinear acoustics, and to [43] for the coupling of Computational Aero Acoustic (CAA) and Computational Fluid Dynamics (CFD) solvers. Moreover, we assume that the flow is potential close to the scattering object and uniform far away from it. This geometric setup leads to a partition of the unbounded medium of propagation into two subdomains, the bounded interior domain near the scattering object where the flow is non-uniform and the unbounded exterior domain far away from the object where the flow is uniform. The main contribution of this work is the reformulation of the convected Helmholtz equation using the Prandtl–Glauert transformation on the whole flow domain, yielding (i) the classical Helmholtz equation in the exterior domain and (ii) an anisotropic diffusive PDE with skew-symmetric first-order perturbation in the interior domain such that its transmission condition at the coupling boundary naturally fits the Neumann condition from the classical Helmholtz equation. The Prandtl–Glauert transformation has been used in [14] for the uniformly convected Helmholtz equation. In the present case where the flow is non-uniform in the interior domain, this reformulation allows us to use efficient off-the-shelf tools to perform a BEM–FEM coupling. Namely, a FEM is utilized in the interior domain to discretize the anisotropic second-order PDE, a BEM is utilized for the classical Helmholtz equation in the exterior domain, and Dirichlet-to-Neumann maps are used for the coupling. We emphasize that the key advantage of using the Prandtl–Glauert transformation is that the BEM part of the resolution only involves integral operators corresponding to the classical Helmholtz equation. We consider two approaches for the coupling, leading, to the authors’ knowledge, to two novel coupled BEM–FEM formulations for the convected Helmholtz equation. The first formulation involves one surface unknown and can be affected by resonant frequencies, while the second one uses the stabilized CIE technique from [8,22], avoids resonant frequencies, and involves two surface unknowns. Our numerical results show that the first formulation yields results polluted by spurious oscillations in the close vicinity of resonant frequencies, whereas the second formulation yields consistent solutions at all frequencies. This advantage of the second formulation is particularly relevant in practice at high frequencies, where the density of resonant frequencies is higher.

We briefly discuss alternative methods from the literature to solve the convected Helmholtz equation in unbounded domains. In some cases with simple geometries, the far-field solution is analytically known [39]. Boundary integral equations involving the Green kernel associated with the convected Helmholtz equation have been derived in [4]. Other numerical methods include infinite finite elements [5,46] and the method of fundamental solutions [16]. An alternative approach to treat unbounded domains is to use Perfectly Matched Layers (PML), combined with a volumic resolution using, e.g., the FEM. Versions of PML for the convected Helmholtz equation are considered in [3,36]. The use of PML allows one to consider unbounded domains of propagation, but the solution is only available within the domain of computation. This can be a drawback in the following situations: (i) when one is interested in the pressure field far away from the scattering object, or (ii) when scattering objects are located far away from each other so that the volumic resolution has to be carried out in a very large area. Instead, with coupled BEM–FEM, the volumic resolution only takes place in the areas where the flow is non-uniform, and the pressure can be retrieved at any point of the exterior domain using known representation formulas, regardless of the distance of this point to the scattering objects. However, coupled BEM–FEM exhibit matrices with dense blocks for the unknowns on the boundary, and an additional treatment is sometimes needed to avoid resonant frequencies. These two points are addressed in this work.

The material is organized as follows: off-the-shelf tools useful to carry out the coupling are recalled in Section 2. The Prandtl–Glauert transformation of the convected Helmholtz equation is derived in Section 3. The coupled variational formulations are obtained in Section 4, and the most salient points in their mathematical analysis are presented. The finite-dimensional approximation of the coupled formulations is addressed in Section 5, along with a discussion on the structure of the linear systems and the algorithms to solve them effectively. Finally, numerical results are presented in Section 6, and some conclusions are drawn in Section 7.

2. Classical tools for BEM–FEM coupling of the classical Helmholtz equation

In this section, the ingredients used to carry out the BEM–FEM coupling are recalled in the context of the classical Helmholtz equation (so that the medium of propagation is at rest).

2.1. Boundary integral operators

Fig. 1 describes the geometric setup considered in this section. Let $\Omega^-\subset \mathbb{R}^3$ be a bounded open set with boundary $\Gamma_\infty^-$, and set $\Omega^+ := \mathbb{R}^3 \setminus \overline{\Omega^-}$. The surface $\Gamma_\infty^-$ is assumed to be Lipschitz. The one-sided Dirichlet traces on $\Gamma_\infty^-$ of a smooth function $u$ in $\Omega^+ \cup \Omega^-$ are defined as $\gamma_0^+ u^+ = u^+|_{\Gamma_\infty^-}$, and the one-sided Neumann traces as $\gamma_1^+ u^+ = (\nabla u^+)|_{\Gamma_\infty^-} \cdot n$, where $u^+ = u|_{\Omega^+}$ and where $n$ is the unit normal vector to $\Gamma_\infty^-$ conventionally pointing towards $\Omega^-$. These trace operators are extended to bounded linear operators $\gamma_0^+ : H^1(\Omega^+) \to H^0(\Gamma_\infty^-)$ and $\gamma_1^+ : H(\Omega^+, \Omega^+) \to H^-^1(\Gamma_\infty^-)$, where $H^0(\Gamma_\infty^-)$ and $H^-^1(\Gamma_\infty^-)$ are the usual Sobolev spaces on $\Gamma_\infty^-$, and $H(\Omega^+, \Omega^+) := \{ v \in H^1(\Omega^+), \Delta v \in L^2(\Omega^+) \}$ (see [42, Lemma 20.2]). It is actually sufficient to consider functional spaces on compact subsets of $\Omega^+$ to define exterior traces on $\Gamma_\infty^-$.

For $u \in H^1(\Omega^+ \cup \Omega^-)$, the jump and average of its Dirichlet traces across $\Gamma_\infty^-$ are defined respectively as $[\gamma_0 u]|_{\Gamma_\infty^-} = \gamma_0^+ u^+ - \gamma_0^- u^-$ and $[\gamma_0 u]|_{\Gamma_\infty^-} = \frac{1}{2}(\gamma_0^+ u^+ + \gamma_0^- u^-)$. For $u \in H(\Omega^+ \cup \Omega^-) := \{ v \in H^1(\Omega^+ \cup \Omega^-), \Delta v \in L^2(\Omega^+ \cup \Omega^-) \}$, the jump and
average of its Neumann traces across $\Gamma_\infty$ are defined respectively as $[\gamma_1 u]|_{\Gamma_\infty} = \gamma_1^+ u^+ - \gamma_1^- u^-$ and $[\gamma_1 u]|_{\Gamma_\infty} = \frac{1}{2}(\gamma_1^+ u^+ + \gamma_1^- u^-)$. When a trace is single-valued on $\Gamma_\infty$, we omit the superscripts $\pm$. Furthermore, the $L^2(\Gamma_\infty)$-inner product $\langle \cdot, \cdot \rangle_{L^2(\Gamma_\infty)} : L^2(\Gamma_\infty) \times L^2(\Gamma_\infty) \to \mathbb{C}$ is defined as $\langle \lambda, \mu \rangle_{L^2(\Gamma_\infty)} = \int_{\Gamma_\infty} \bar{\lambda}(y) \mu(y) ds(y)$, where $\bar{\cdot}$ denotes the complex conjugate, and is extended to a duality pairing on $H^{-\frac{1}{2}}(\Gamma_\infty) \times H^\frac{1}{2}(\Gamma_\infty)$ denoted by $\langle \cdot, \cdot \rangle_{H^{-\frac{1}{2}}(\Gamma_\infty), H^\frac{1}{2}(\Gamma_\infty)}$. We then define the product

$$\langle \lambda, \mu \rangle_{\Gamma_\infty} = \begin{cases} 
\langle \lambda, \mu \rangle_{H^{-\frac{1}{2}}(\Gamma_\infty), H^\frac{1}{2}(\Gamma_\infty)} & \text{if } \lambda \in H^{-\frac{1}{2}}(\Gamma_\infty), \, \mu \in H^\frac{1}{2}(\Gamma_\infty), \\
\langle \mu, \lambda \rangle_{H^{-\frac{1}{2}}(\Gamma_\infty), H^\frac{1}{2}(\Gamma_\infty)} & \text{if } \lambda \in H^\frac{1}{2}(\Gamma_\infty), \, \mu \in H^{-\frac{1}{2}}(\Gamma_\infty).
\end{cases}$$  \hfill (1)

Consider the following equations:

$$\Delta u + k^2 u = 0 \quad \text{in } \Omega^+ \cup \Omega^-,$$ \hfill (2a)

$$\lim_{r \to +\infty} r \left( \frac{\partial u}{\partial r} - iku \right) = 0,$$ \hfill (2b)

where $k$ is the wave number. A function solving (2a) is said to be a piecewise Helmholtz solution and a function solving (2a)-(2b) is said to be a radiating piecewise Helmholtz solution. The condition at infinity (2b) is the Sommerfeld radiation condition, that guarantees existence and uniqueness for Helmholtz exterior problems [35, Theorem 9.10].

For all $\lambda \in C^0(\Gamma_\infty)$, the single-layer potential is defined as $S(\lambda) = \int_{\Gamma_\infty} E(y - x) \lambda(y) ds(y)$, $x \in \mathbb{R}^3 \setminus \Gamma_\infty$, where $E(x) = \frac{\exp(ik|x|)}{4\pi|x|}$ is the fundamental solution of (2a)-(2b). For all $\mu \in C^0(\Gamma_\infty)$, the double-layer potential is defined as $D(\mu) = \int_{\Gamma_\infty} \nabla_y E(y - x) \mu(y) ds(y)$, $x \in \mathbb{R}^3 \setminus \Gamma_\infty$. From [41, Theorem 3.1.16], these operators can be extended to bounded linear operators $S : H^{-\frac{1}{2}}(\Gamma_\infty) \to H^{1}_\text{loc}(\mathbb{R}^3)$ and $D : H^\frac{1}{2}(\Gamma_\infty) \to H^{1}_\text{loc}(\mathbb{R}^3 \setminus \Gamma_\infty)$ where, for any open set $X$, $H^{1}_\text{loc}(X) = \{u \in H^1(K), \forall K \subset X\}$ compact. Moreover, both operators map onto radiating piecewise Helmholtz solutions. Recalling [26, Theorem 3.1.1], a radiating piecewise Helmholtz solution $u$ can be represented from its Dirichlet and Neumann jumps across $\Gamma_\infty$ in the form

$$u = -S([\gamma_1 u]|_{\Gamma_\infty}) + D([\gamma_0 u]|_{\Gamma_\infty}) \quad \text{in } \Omega^+ \cup \Omega^-.$$ \hfill (3)

The operators

$$S : H^{-\frac{1}{2}}(\Gamma_\infty) \to H^\frac{1}{2}(\Gamma_\infty), \quad S\lambda = \gamma_0(S\lambda),$$

$$D : H^\frac{1}{2}(\Gamma_\infty) \to H^{\frac{1}{2}}(\Gamma_\infty), \quad D\mu = \{\gamma_0(D\mu)\}|_{\Gamma_\infty},$$

$$\bar{D} : H^{-\frac{1}{2}}(\Gamma_\infty) \to H^{-\frac{1}{2}}(\Gamma_\infty), \quad \bar{D}\lambda = \{\gamma_1(S\lambda)\}|_{\Gamma_\infty},$$

$$N : H^\frac{1}{2}(\Gamma_\infty) \to H^{-\frac{1}{2}}(\Gamma_\infty), \quad N\mu = -\gamma_1(D\mu),$$ \hfill (4)
sections 2.3 and 2.4 below. From the second line of (9), let now $F$ be the function defined by $v|_{\Omega^+} = u - u_{\text{inc}}$ and $v|_{\Omega^-} = -u_{\text{inc}}$. The function $v$ is a radiating piecewise Helmholtz solution (this follows from (6b) and (6e) on $\Omega^+$, and from (7) on $\Omega^-$). Moreover, since the field $u_{\text{inc}}$ is continuous across $\Gamma_{\infty}$,

$$\Delta u_{\text{inc}} + k^2 u_{\text{inc}} = 0 \quad \text{in} \quad \Omega^-.$$  

Consider the following transmission problem:

$$F(u) = 0 \quad \text{in} \quad \Omega^-,$$

$$\Delta(u - u_{\text{inc}}) + k^2(u - u_{\text{inc}}) = 0 \quad \text{in} \quad \Omega^+,$$

$$\gamma_0^+ u^+ - \gamma_0^- u^- = 0 \quad \text{on} \quad \Gamma_{\infty},$$

$$\gamma_1^+ u^+ - \gamma_1^- u^- = 0 \quad \text{on} \quad \Gamma_{\infty},$$

$$\lim_{r \to +\infty} r \left( \frac{\partial(u - u_{\text{inc}})}{\partial r} - ik(u - u_{\text{inc}}) \right) = 0,$$

where $F$ denotes some differential operator and $u_{\text{inc}}$ is an incident acoustic field. The field $u_{\text{inc}}$ is created by a source located in $\Omega^+$, and solves the classical Helmholtz equation outside the support of this source. In particular,

$$\Delta u_{\text{inc}} + k^2 u_{\text{inc}} = 0 \quad \text{in} \quad \Omega^-.$$  

Let now $u$ be the function defined by $v|_{\Omega^+} = u - u_{\text{inc}}$ and $v|_{\Omega^-} = -u_{\text{inc}}$. The function $v$ is a radiating piecewise Helmholtz solution (this follows from (6b) and (6e) on $\Omega^+$, and from (7) on $\Omega^-$). Moreover, since the field $u_{\text{inc}}$ is continuous across $\Gamma_{\infty}$,

$$\gamma_0^- u^- = \gamma_0^+(u - u_{\text{inc}})^++ \gamma_0^+ u_{\text{inc}} = \gamma_0^+(u - u_{\text{inc}})^++ \gamma_0^+ u_{\text{inc}} = \gamma_0^+ u^+.$$  

Likewise, $[\gamma_1 v]_{\Gamma_{\infty}} = \gamma_1^+ u^+$. Then, (5) applied to $v$ yields

$$\begin{pmatrix} \frac{1}{2} I - D & S \\ N & \frac{1}{2} I + \tilde{D} \end{pmatrix} \begin{pmatrix} \gamma_0 u \\ \gamma_1 u \end{pmatrix} = \begin{pmatrix} \gamma_0 u_{\text{inc}} \\ \gamma_1 u_{\text{inc}} \end{pmatrix}.$$  

A DtN operator maps any function $\theta$ to the Neumann trace $\gamma_1 u$ where $u$ solves the exterior Helmholtz problem, with $\gamma_0 \theta = \theta$ as Dirichlet boundary condition on $\Gamma_{\infty}$. Various DtN maps can be derived from (9). Two examples are detailed in Sections 2.3 and 2.4 below.

### 2.3. An unstable DtN map

Using the first line of (9), $\gamma_1 u = S^{-1}((D - \frac{1}{2} I)(\gamma_0 u) + \gamma_0 u_{\text{inc}})$. At this point, the inverse of $S$ is written formally. Conditions of inversibility are discussed below. From the second line of (9), $\gamma_1 u = -N(\gamma_0 u) + (\frac{1}{2} I - \tilde{D})(\gamma_1 u) + \gamma_1 u_{\text{inc}}$. Injecting into the right-hand side of this relation the expression of $\gamma_1 u$ derived above yields the DtN affine map: $D_{\text{DtN}_{\text{unstab}}} : H^{\frac{1}{2}}(\Gamma_{\infty}) \rightarrow H^{-\frac{1}{2}}(\Gamma_{\infty})$ such that

$$D_{\text{DtN}_{\text{unstab}}} (\gamma_0 u) = -N(\gamma_0 u) + \left( \frac{1}{2} I - \tilde{D} \right) (\lambda) + \gamma_1 u_{\text{inc}},$$  

where the auxiliary field $\lambda \in H^{-\frac{1}{2}}(\Gamma_{\infty})$ is such that

$$\left( D - \frac{1}{2} I \right)(\gamma_0 u) - S \lambda = -\gamma_0 u_{\text{inc}}.$$  

The main difficulty with the map (10) stems from the fact that $\ker(S)$ depends on whether $-k^2$ belongs to the set $\Lambda$ of Dirichlet eigenvalues for the Laplacian on the bounded domain $\Omega^-$. Specifically, $\ker(S) = \{0\}$ if $-k^2 \notin \Lambda$, while $\ker(S)$ contains nontrivial elements if $-k^2 \in \Lambda$.

### Remark 2.1.

The $D_{\text{DtN}_{\text{unstab}}}$ affine map was proposed by Costabel to obtain a symmetric coupling in the case of self-adjoint operators [12]. The $D_{\text{DtN}_{\text{unstab}}}$ map can be well-defined for certain operators, for instance for transmission problems for the Laplace equation, the unstability being here linked to the specificity of the Helmholtz equation.
2.4. A stable DtN map

The idea of considering a linear combination of $S$ and $\frac{1}{2}I + D$ to derive well-posed boundary integral equations was independently proposed by Brakhage and Werner [6], Leis [28] and Panich [38]. This is the so-called Combined Field Integral Equation (CFIE). However, $S$ and $D$ map $H^{-\frac{1}{2}}(I_\infty)$ into different spaces ($H^{\frac{1}{2}}(I_\infty)$ and $H^{-\frac{1}{2}}(I_\infty)$ respectively). This inconsistency in the functional setting can be solved by considering a regularizing compact operator from $H^{-\frac{1}{2}}(I_\infty)$ into $H^{\frac{1}{2}}(I_\infty)$, as observed by Buffa and Hiptmair [8].

We briefly recall the approach of [8]. Let $\nabla r_\infty$ denote the surfacic gradient on $I_\infty$. Consider the following Hermitian sesquilinear form: For all $p, q \in H^1(I_\infty)$,

$$\delta r_\infty(p, q) = (\nabla r_\infty p, \nabla r_\infty q)_{r_\infty} + (p, q)_{r_\infty},$$

and the regularizing operator $M : H^{-1}(I_\infty) \rightarrow H^{1}(I_\infty)$ defined through the following implicit relation: For all $p \in H^1(I_\infty)$, $\delta r_\infty(M p, q) = (p, q)_{r_\infty}$ for all $q \in H^1(I_\infty)$. It is readily seen that $M = (-\Delta r_\infty + I)^{-1}$, where $\Delta r_\infty$ is the Laplace–Beltrami operator on $I_\infty$. Many choices of DtN maps based on CFIE strategies with the regularizing operator $M$ lead to well-posed systems whatever the value of $k$. The present choice hinges on the inversion of the operator $S + i\eta M(\frac{1}{2}I + D)$ mapping $H^{-\frac{1}{2}}(I_\infty)$ into $H^{\frac{1}{2}}(I_\infty)$ since, from [8, Lemma 4.1], this operator is bijective as long as the coupling parameter $\eta$ is such that Re$(\eta) \neq 0$. To do so, the first line of (9) and the application of $M$ to the second line of (9) are used to obtain

$$(I + D) + i\eta MN S + i\eta M(\frac{1}{2}I + D)\left(\begin{array}{c} \gamma_0u \\ \gamma_0u + i\eta M \gamma_1 u_{inc} \end{array}\right) = \left(\begin{array}{c} \gamma_0u_{inc} + i\eta M \gamma_1 u_{inc} \\ \gamma_1 u_{inc} \end{array}\right).$$

Then, using both equations in (13) in the same fashion as in Section 2.3 leads to $DtN_{stab} : H^{\frac{1}{2}}(I_\infty) \rightarrow H^{-\frac{1}{2}}(I_\infty)$ such that

$$DtN_{stab}(\gamma_0 u) = N(\gamma_0 u) + \left(\frac{1}{2}I - D\right)(\lambda) + \gamma_1 u_{inc},$$

where $\lambda \in H^{-\frac{1}{2}}(I_\infty)$ is such that

$$S(\lambda) + \left(\frac{1}{2}I - D\right)(\gamma_0 u) + i\eta p = \gamma_0 u_{inc},$$

and $p \in H^1(I_\infty)$ is such that for all $q \in H^1(I_\infty)$,

$$\delta r_\infty(p, q) = (N(\gamma_0 u), q)_{r_\infty} + \left(\frac{1}{2}I + D\right)(\lambda), q)_{r_\infty} - (\gamma_1 u_{inc}, q)_{r_\infty}.$$

3. The aeroacoustic problem

This section describes the problem of acoustic scattering by a solid object in a non-uniform convective flow, together with the underlying physical assumptions.

3.1. Notation and preliminaries

Fig. 2 describes the geometric setup. The interior domain, corresponding to the area near the scattering object where the convective flow is non-uniform, is denoted by $\Omega^-$. In the exterior domain, $\Omega^+$, the convective flow is assumed to be uniform. The complete medium of propagation, denoted by $\Omega \subset \mathbb{R}^3$, is such that $\Omega = \Omega^+ \cup \Omega^- \cup \Gamma_\infty = \mathbb{R}^3 \setminus \{\text{solid object}\}$, where $\Gamma_\infty = \partial \Omega^+ \cap \partial \Omega^-$ is the boundary between the interior and exterior domains. The surface $\Gamma_\infty$ is assumed to be Lipschitz. Such an assumption is sufficiently large to include for instance polyhedric surfaces resulting from the use of a finite element mesh in $\Omega$. The surface of the solid scattering object, denoted by $\Gamma = \partial \Omega^- \setminus \Gamma_\infty$, is assumed to be Lipschitz. The source term $g$ is time-harmonic with pulsation $\omega$ and is assumed to be located in $\Omega^+$. Typically, this source term can be an acoustic monopole located at $x_s \in \Omega^+$ of amplitude $A_s$, so that $g = A_s \delta_{x_s}$, where $\delta_{x_s}$ denotes the Dirac mass distribution at $x_s$.

The speed of sound when the medium of propagation is at rest is denoted by $c$, the wave number by $k$, the density by $\rho$, and the acoustic velocity and pressure, respectively, by $v$ and $p$. The rescaled velocity is defined as $M = c^{-1} v$, where $M = |M|$ is the Mach number. The subscript $\infty$ refers to uniform flow quantities related to $\Omega^+$, whereas the subscript $0$ refers to point-dependent flow quantities related to $\Omega^-$, that is, $\rho_{\Omega^+} = \rho_0(x)$, $\rho_{\Omega^-} = \rho_\infty$, $k_{\Omega^+} = k_0(x)$, $k_{\Omega^-} = k_\infty$, $c_{\Omega^+} = c_0(x)$, $c_{\Omega^-} = c_\infty$, $M_{\Omega^+} = M_0(x)$, and $M_{\Omega^-} = M_\infty$. The convective flow is continuous through $\Gamma_\infty$ and tangential on $\Gamma$. Hence, $\rho$, $k$, and $M$ are continuous through $\Gamma_\infty$, and $M \cdot n = 0$ on $\Gamma$.

The physical quantities are associated with complex quantities with the following convention on, for instance, the acoustic pressure: $p \leftrightarrow \text{Re}(p \exp(-i\omega t))$. In what follows, we always refer to the complex quantity. Furthermore, the Hermitian product of two vectors $U, W \in \mathbb{C}^3$ is denoted by $U \cdot W = \sum_{i=1}^3 \bar{U}_iW_i$, and the associated Euclidean norm in $\mathbb{C}^3$ is denoted by $\| \cdot \|$.
3.2. The convected Helmholtz equation

In the interior domain $\Omega^-$, the convective flow is supposed to be stationary, inviscid, isentropic, potential and subsonic. The acoustic effects are considered to be a first-order perturbation of this flow. With these assumptions, there exists an acoustic potential $\varphi$ such that $\mathbf{v} = \nabla \varphi$.

Following [23, Eq. (F27)] and [19], and making use of the acoustic potential, the linearization of the Euler equations leads to

$$
\rho \left( k^2 \varphi + ik \mathbf{M} \cdot \nabla \varphi \right) + \nabla \cdot \left( \rho \left( \nabla \varphi - (\mathbf{M} \cdot \nabla \varphi) \mathbf{M}\right) + ik \mathbf{M} \cdot \nabla \varphi \right) = g \quad \text{in} \; \Omega^-.
$$

where $\varphi$ is the unknown acoustic potential, and $\rho$, $k$, $\mathbf{M}$, and $g$ are known. Eq. (17) is the convected Helmholtz equation. Under the assumption that the acoustic perturbations are perfectly reflected by the solid object, the acoustic potential verifies an homogeneous Neumann boundary condition on $\Gamma$:

$$
\nabla \varphi \cdot \mathbf{n} = 0 \quad \text{on} \; \Gamma.
$$

Problem (17)–(18) is completed by a Sommerfeld-like boundary condition at infinity.

In the exterior domain $\Omega^+$ where the flow quantities are uniform, Eq. (17) becomes

$$
\Delta \varphi + k^2 \varphi + 2ik \mathbf{M}_\infty \cdot \nabla \varphi - \mathbf{M}_\infty \cdot \nabla (\mathbf{M}_\infty \cdot \nabla \varphi) = g \quad \text{in} \; \Omega^+.
$$

If there were no scattering object and if the convective flow were uniform in $\mathbb{R}^3$ (and thus equal to the flow at infinity), the source term $g$ would create an acoustic potential denoted by $\varphi_{inc}$ in $\mathbb{R}^3$. This potential, which solves (19) in $\mathbb{R}^3$, has an analytical expression, and $\varphi_{inc}$ and $\mathbf{n} \cdot \nabla \varphi_{inc}$ are continuous across $\Gamma_\infty$. The acoustic potential scattered by the solid object is defined as $\varphi_{sc} = \varphi - \varphi_{inc}$ in $\Omega^+$. Eliminating the known acoustic potential $\varphi_{inc}$ created by the source yields

$$
\Delta \varphi_{sc} + k^2 \varphi_{sc} + 2ik \mathbf{M}_\infty \cdot \nabla \varphi_{sc} - \mathbf{M}_\infty \cdot \nabla (\mathbf{M}_\infty \cdot \nabla \varphi_{sc}) = 0 \quad \text{in} \; \Omega^+.
$$

3.3. The Prandtl–Glauert transformation

The Prandtl–Glauert transformation was introduced by Glauert [18] to study the compressible effects of the air on the lift of an airfoil and was applied to subsonic aeroacoustic problems by Amiet and Sears [2]. Herein, the Prandtl–Glauert transformation is applied in the complete medium of propagation and is based on the reduced velocity $\mathbf{M}_\infty$. This transformation consists in changing the space and time variables as

$$
\begin{align*}
\mathbf{x}' &= y_\infty (\mathbf{M}_\infty \cdot \mathbf{x}) \mathbf{M}_\infty + \left( \mathbf{x} - (\mathbf{M}_\infty \cdot \mathbf{x}) \mathbf{M}_\infty \right), \quad \mathbf{x} \in \Omega, \\
t' &= t - \frac{y_\infty^2}{c_\infty} \mathbf{M}_\infty \cdot \mathbf{x}, \quad t \in \mathbb{R},
\end{align*}
$$

where $y_\infty$ is the infinite Mach number and $c_\infty$ is the infinite sound speed.
where \( \gamma_\infty = \frac{1}{\sqrt{1 - M_\infty^2}} \) and \( \hat{M}_\infty = M_\infty^{-1} \hat{M}_\infty \) with \( M_\infty = |M_\infty| \). The spatial transformation corresponds to a dilatation along \( \hat{M}_\infty \) of magnitude \( \gamma_\infty \), the component orthogonal to \( \hat{M}_\infty \) being unchanged. In what follows, we suppose that the flow is subsonic everywhere, so that \( M_\infty < 1 \). Under this property, the Prandtl–Glauert transformation is a \( C^\infty \)-diffeomorphism from \( \Omega \times \mathbb{R} \) to \( \Omega' \times \mathbb{R} \), where \( \Omega' \) denotes the transformed medium of propagation.

### 3.4. The transformed problem

To apply the Prandtl–Glauert transformation to a PDE in the frequency domain, one has to change the differential operators as

\[
\nabla u = N' \nabla' u, \quad \nabla \cdot U = \nabla' \cdot N' U,
\]

for a scalar-valued function \( u \) and a vector-valued function \( U \). Here, \( N' = I + C_\infty \hat{M}_\infty M_\infty^T \) with \( C_\infty = \frac{\gamma_\infty^{-1}}{M_\infty} \) and \( \nabla' \) refers to derivatives with respect to the transformed variables \( x' \). Moreover, it is readily verified that

\[
N' M = M + C_\infty P M_\infty, \quad N' M_\infty = \gamma_\infty M_\infty, \quad N' M_\infty M = N' M_\infty = M = \gamma_\infty P,
\]

where \( P = M \cdot M_\infty \). Dividing Eq. (17) by \( \rho_\infty \) and applying (22) leads to

\[
\rho_\infty^2 \varphi + i r k \cdot M \cdot \nabla' \varphi + \nabla' \cdot (r \cdot n' \cdot N' \nabla' \varphi) = -\nabla' \cdot (r \cdot \nabla' \cdot \varphi M' + \nabla' \cdot (r k \cdot \nabla' \cdot \varphi M')) = \rho_\infty^{-1} g,
\]

where \( r = \frac{x}{\rho_\infty} \). Let \( f \) be such that \( \varphi(x) = \alpha(x) f(x') \) with \( \alpha(x') = \exp(-i k_\infty \gamma_\infty (M_\infty \cdot x')) \), \( x' \in \Omega' \): \( f_\text{inc} \) and \( f_\text{sc} \) are defined from \( \varphi_\text{inc} \) and \( \varphi_\text{sc} \) in the same fashion, so that \( f_\text{inc} \) is analytically known, and defined in \( \mathbb{R}^3 \). Expanding the derivatives with respect to \( \alpha \) and using (23) leads to

\[
\alpha^2 f + i r k \cdot M \cdot \nabla' f + \alpha k \cdot q f + \nabla' \cdot (\alpha r k \cdot \nabla' f) + \nabla' \cdot (\alpha k^2 f) \cdot M = \rho_\infty^{-1} g.
\]

where \( q = \gamma_\infty^2 \frac{K_0}{k_\infty} \) and where we used the fact that \( \nabla' \alpha = -\alpha i k_\infty \gamma_\infty M_\infty \). Expanding again the derivatives with respect to \( \alpha \) and using again (23) as well as the symmetry of \( N' \), we infer after some calculations that

\[
\rho_\infty^2 \beta f + i r k \cdot V \cdot \nabla' f + \nabla' \cdot \left( i r k \cdot V + r \cdot \Xi \cdot \nabla' f \right) = \zeta \quad \text{in} \ \Omega',
\]

where \( \beta = (1 + q) = q^2 M_\infty^2 \), \( V = (1 + q) M' - q \gamma_\infty M_\infty \), \( \Xi = N' \nabla' N' \) with \( O = I - M M^T \), and \( \zeta(x') = \rho_\infty^{-1} \alpha^{-1} \gamma_\infty \gamma_\infty \gamma_\infty \).

Consider now the boundary condition (18). The normals on the initial geometry are denoted by \( n \), and the normals on the transformed geometry by \( n' \). It is readily seen that

\[
\nabla = K_\infty N' n',
\]

where \( K_\infty \) is a normalization factor that is not needed in what follows. Owing to (22) and (25), (18) becomes \( \nabla' \varphi = -i k_\infty \gamma_\infty N' \nabla' f \), and \( \varphi_\text{inc} = \nabla' \cdot (\alpha k_\infty \gamma_\infty M') \cdot n' = 0 \). Since the flow is tangential on \( \Gamma' \), \( M \cdot n' = 0 \) on \( \Gamma' \). Hence, \( M \cdot N' n' = 0 \) on \( \Gamma' \), where \( \Gamma' \) denotes the transformed boundary \( \Gamma' \), so that

\[
\left( \nabla' \nabla' f - (N' M' \cdot \nabla' f) + i k_\infty \gamma_\infty N' \right) \cdot N' n' = 0.
\]

Using the symmetry of \( N' \) and (23), (26) leads to

\[
(ik r k \cdot V + r \cdot \Xi \cdot \nabla' f) \cdot n' = 0 \quad \text{on} \ \Gamma'.
\]

Notice that although the term \( M \cdot N' n' \) vanishes, it has been added to the expression of the boundary condition in order to obtain in (27) the normal component of the vector-valued function in the divergence term of (24). This point is crucial to derive coupled formulations.

In what follows, primes are omitted for brevity, and the transformed geometry, unknowns, and operators are considered. In summary, the transformed convected Helmholtz equation together with the boundary condition and radiation condition at infinity takes the form

\[
\rho_\infty^2 \beta f + i r k \cdot V \cdot \nabla f + \nabla \cdot (i r k \cdot V + r \cdot \Xi \cdot \nabla f) = \zeta \quad \text{in} \ \Omega',
\]

\[
(ik r k \cdot V + r \cdot \Xi \cdot \nabla f) \cdot n = 0 \quad \text{on} \ \Gamma',
\]

\[
\lim_{r \to \infty} \left( \frac{\partial f - f_\text{inc}}{\partial r} - i k_\infty (f - f_\text{inc}) \right) = 0,
\]

where \( f \) is searched in \( H^1_{\text{loc}}(\Omega) \). The Sommerfeld radiation condition (28c) is written for the scattered potential, since some incident acoustic potentials, e.g., plane waves, do not verify it.
Proposition 3.1. The matrix $\Xi$ is symmetric positive definite in $\Omega^-$ with
$$
\Xi \cdot U \geq (1 - M_0^2) \|U\|^2 \quad \text{for all } U \in \mathbb{C}^3,
$$
where $M_0$ is uniformly bounded away from 1 since the convective flow is assumed to be subsonic. Moreover, still in $\Omega^-$.\[\Xi \cdot W \leq \frac{1 + M_0^2}{1 - M_\infty^2} \|U\| \|W\| \quad \text{for all } U, W \in \mathbb{C}^3.\]

An important observation is that in $\Omega^+$, $\beta = \gamma^2_{\infty}$. $\mathbf{V} = \mathbf{0}$ and $\Xi = I$, so that (28a) becomes
$$
\Delta f + \hat{k}_\infty^2 f = \zeta \quad \text{in } \Omega^+,
$$
where
$$\hat{k}_\infty = \gamma_{\infty} k_{\infty}.\]

Moreover, since supp($\zeta$) $\subset \Omega^+$, $f_{\text{inc}}$ satisfies
$$\Delta f_{\text{inc}} + \hat{k}_\infty^2 f_{\text{inc}} = \zeta \quad \text{in } \Omega^+, \quad \Delta f_{\text{inc}} + \hat{k}_\infty^2 f_{\text{inc}} = 0 \quad \text{in } \mathbb{R}^3 \setminus \Omega^+.\]

Eliminating $f_{\text{inc}}$ in (31) yields
$$\Delta f_{\text{sc}} + \hat{k}_\infty^2 f_{\text{sc}} = 0 \quad \text{in } \Omega^+.\]

This is the classical Helmholtz equation with modified wave number $\hat{k}_\infty$.

4. Coupling procedure

The purpose of this section is to derive two BEM–FEM coupled formulations for problem (28) using the tools presented in Section 2 and to analyze their well-posedness.

4.1. The transmission problem

We consider the following transmission problem:
$$
\begin{align*}
2 \beta f^- + i r k \mathbf{V} \cdot \nabla f^- &+ \nabla \cdot (i r k \mathbf{V} + r \Xi \nabla f) = 0 \quad \text{in } \Omega^-; \\
\Delta f_{\text{sc}} + \hat{k}_\infty^2 f_{\text{sc}} &= 0 \quad \text{in } \Omega^+, \\
(irk \mathbf{V} + r \Xi \nabla f) \cdot \mathbf{n} &= 0 \quad \text{on } \Gamma, \\
\gamma_0^+ f^+ - \gamma_0^- f^- &= 0 \quad \text{on } \Gamma^0, \\
\gamma_1^+ f^+ - \gamma_1^- f^- &= 0 \quad \text{on } \Gamma^1, \\
\lim_{r \to +\infty} r \left( \frac{\partial (f^+ - f_{\text{inc}})}{\partial r} - i k_{\infty} (f^+ - f_{\text{inc}}) \right) &= 0.
\end{align*}
$$

It is easily seen that problem (28) is equivalent to problem (35).

Proposition 4.1. Problem (35) has at most one solution in $H^1_{\text{loc}}(\Omega)$.

We give the proof since the non-uniform convection coefficients do not have enough regularity to apply the classical argument of analytical continuation.

Proof. Suppose $\zeta = 0$, so that $f_{\text{inc}} = 0$, and let $f \in H^1_{\text{loc}}(\Omega)$ solve (35). Then, $f$ solves (28). Let $B$ be an open ball containing $\Omega^-$. Let $f^i \in H(\Delta, B)$. Using Green’s first identity,
$$
\begin{align*}
0 &= \int_{\Omega^\infty B} (-rk^2 \beta \tilde{f}^- - ikr \mathbf{V} \cdot \nabla \tilde{f}^- - \nabla \cdot (irk \mathbf{V} + r \Xi \nabla \tilde{f})) f^i \\
&= \int_{\Omega^\infty B} r \Xi \nabla \tilde{f} \cdot \nabla f^i - rk^2 \beta \tilde{f}^- f^i - ikr \mathbf{V} \cdot (\nabla \tilde{f}^- f^i - \nabla f^i \tilde{f}) - (\gamma_0^- f \cdot \gamma_0^- f^i)_{\partial B},
\end{align*}
$$

where $\gamma_0^- f$ and $\gamma_1^- f$ are the Dirichlet and Neumann traces on $\partial B$ from $B$. Taking $f^i = f$ yields
so that \( \text{Im}(\gamma_{1,ab}f, \gamma_{0,ab}f)_{ab} = 0 \). Using Rellich Lemma (see [35, Lemma 9.9]), since \( f \in H^{1}_{\text{loc}}(\mathbb{R}^{3} \setminus \mathcal{B}) \) solves the classical Helmholtz equation in \( \mathbb{R}^{3} \setminus \mathcal{B} \) and satisfies the Sommerfeld radiation condition, as well as \( \text{Im}(\gamma_{1,ab}f, \gamma_{0,ab}f)_{ab} \geq 0 \), it is inferred that \( f|_{\Omega \cap \mathcal{B}} \equiv 0 \). Eq. (28a) can be written

\[
L(f) := (rk^{2}\beta + \nabla \cdot (irkV))f + 2irkV \cdot \nabla f + \nabla \cdot (r\nabla f) = 0 \quad \text{in} \ \Omega.
\]

From [17, Theorem 1.1], since \( r\mathcal{E} \) is uniformly elliptic with Lipschitz continuous coefficients, and \( rk^{2}\beta + \nabla \cdot (irkV) \) and \( 2irkV \) have bounded coefficients, the differential operator \( L \) satisfies the strong unique continuation property in \( \Omega \). Hence, \( f|_{\Omega} \equiv 0 \) implies that \( f|_{\Omega} \equiv 0 \). □

4.2. Weak formulation in the interior domain \( \Omega^{-} \)

Let \( \Phi = f|_{\Omega^{-}} \) where \( f \) solves (35). Multiplying (35a) by a test function \( \Phi^{t} \in H^{1}(\Omega^{-}) \) and using a Green formula together with the sesquilinear form (35c) yields

\[
\mathcal{V}(\Phi, \Phi^{t}) - (\gamma_{1}^{-} \Phi, \gamma_{0}^{-} \Phi^{t})_{f_{\infty}} = 0,
\]

with the sesquilinear form

\[
\mathcal{V}(\Phi, \Phi^{t}) = \int_{\Omega^{-}} r\mathcal{E} \nabla \Phi^{\ast} \cdot \nabla \Phi^{t} - \int_{\Omega^{-}} rk^{2} \beta \Phi^{t} - i \int_{\Omega^{-}} rkV \cdot (\Phi \nabla \Phi^{t} - \Phi^{t} \nabla \Phi). \tag{40}
\]

Using the transmission conditions (35d)-(35e), \( \gamma_{0}^{-} \Phi = \gamma_{0}f \) and \( \gamma_{1}^{-} \Phi = \gamma_{1}f \), so that the coupling with the exterior problem can be written as \( \gamma_{1}^{-} \Phi = \text{DtN}(\gamma_{0}^{-} \Phi) \). This yields the following coupled formulation: Find \( \Phi \in H^{1}(\Omega^{-}) \) such that \( \mathcal{V}(\Phi, \Phi^{t}) \in H^{1}(\Omega^{-}) \),

\[
\mathcal{V}(\Phi, \Phi^{t}) - (\text{DtN}(\gamma_{0}^{-} \Phi), \gamma_{0}^{-} \Phi^{t})_{f_{\infty}} = 0. \tag{41}
\]

The coupling is carried out by taking as \( \text{DtN} \) map in (41) the maps presented in Sections 2.3 and 2.4. We recall that Helmholtz equations, as well as corresponding boundary integral operators, are written on a geometry and for unknown functions that have been transformed by the Prandtl–Glaubert transformation; the wave number of the source is \( \hat{k}_{\infty} = \gamma_{\infty}k_{\infty} \) (see (32)).

4.3. Unstable coupled formulation with one surface unknown

Injecting \( \text{DtN}_{\text{unstab}}(\gamma_{0}^{-} \Phi) \) from (10) into the formulation (41) yields, using (11), the following variational formulation: Find \( (\Phi, \lambda) \in \mathcal{H} \) such that,

\[
\mathcal{V}(\Phi, \Phi^{t}) + (N(\gamma_{0}^{-} \Phi), \gamma_{0}^{-} \Phi^{t})_{f_{\infty}} + \left( \left( D - \frac{1}{2} I \right)(\lambda), \gamma_{0}^{-} \Phi^{t} \right)_{f_{\infty}} = (\gamma_{1}f_{\text{inc}}, \gamma_{0}^{-} \Phi^{t})_{f_{\infty}}, \tag{42a}
\]

\[
\left( \left( D - \frac{1}{2} I \right)(\gamma_{0}^{-} \Phi), \lambda^{t} \right)_{f_{\infty}} - (S(\lambda), \lambda^{t})_{f_{\infty}} = -(\gamma_{0}f_{\text{inc}}, \lambda^{t})_{f_{\infty}}. \tag{42b}
\]

with product space \( \mathcal{H} = H^{1}(\Omega^{-}) \times H^{-\frac{1}{2}}(f_{\infty}) \) and inner product \( ((\Phi, \lambda), (\Phi^{t}, \lambda^{t}))_{\mathcal{H}} = (\Phi, \Phi^{t})_{H^{1}(\Omega^{-})} + (\lambda, \lambda^{t})_{H^{-\frac{1}{2}}(f_{\infty})} \).

If \( f \) solves (35), then \( (f^{-}, \gamma^{-} f) \) solves (42), and more generally, \( (f^{-}, \gamma_{1}^{-} f + \lambda^{t}) \) solves (42) for all \( \lambda^{t} \in \ker(S) \). Hence, in the case of resonant frequencies, i.e., \( \hat{k}^{-}_{\infty} \in \Lambda \), where \( \ker(S) \) is not trivial, (42) admits infinitely many solutions. Conversely, if \( (\Phi, \lambda) \) solves (42), then \( \mathcal{R}(\Phi, \lambda) \) solves (35), where \( \mathcal{R} : \mathcal{H} \rightarrow H^{1}_{\text{loc}}(\Omega \setminus f_{\infty}) \) is such that \( \mathcal{R}(\Phi, \lambda)|_{\Omega} = \Phi \) and \( \mathcal{R}(\Phi, \lambda)|_{\Omega^{-}} = \left(-S(\lambda) + D(\gamma_{0}^{-} \Phi) + f_{\text{inc}}\right)|_{f_{\infty}} \). Notice that \( \mathcal{R}(0, \lambda^{t}) = 0 \) for all \( \lambda^{t} \in \ker(S) \). Thus, in the case of resonant frequencies, where (42) admits infinitely many solutions, all of these solutions produce the same solution of (35). However, we will see in Section 6 that the numerical procedure to approximate (42) becomes ill-conditioned so that \( \mathcal{R}(\Phi, \lambda) \) is dominated by numerical errors. For this reason, the formulation (42) is called unstable.

**Theorem 4.2.** If \( \hat{k}^{-2}_{\infty} \notin \Lambda \), problem (42) is well-posed.

**Proof.** The proof is omitted since it proceeds in the same fashion as that of Theorem 4.4 below. □
Remark 4.3 (Symmetry of the system). In the system (42), the only non-symmetric contribution results from the vector $\mathbf{V}$ in the sesquilinear form $\mathcal{V}$, cf. (40). The system becomes symmetric when the flow is uniform everywhere. Notice that this is not an Hermitian symmetry. The operators $D$ and $D$ are dual but not adjoint.

4.4. Stable coupled formulation with two surface unknowns

Injecting $DtN_{\text{stab}}(\gamma_0 \Phi)$ from (14) into the formulation (41) yields, using (15) and (16), the following variational formulation: Find $(\Phi, \lambda, p) \in \mathbb{H}$ such that $\mathcal{V}(\Phi', \lambda', p') \in \mathbb{H}_t$, where

$$\mathcal{V}(\Phi, \Phi') = \int_{\Omega} r \mathbf{v} \cdot \mathbf{v} \Phi' + \int_{\partial \Omega} N^0(\gamma_0^- \Phi), (\gamma_0^- \Phi') d\Gamma_{\infty} + \int_{\Omega} S^0(\lambda^0, \lambda') d\Omega_{\infty} + \delta_{\Gamma_{\infty}}(p, p')$$

with product space $\mathbb{H} = H^1(\Omega^-) \times H^{-\frac{1}{2}}(\Gamma_{\infty}) \times H^1(\Gamma_{\infty})$ and inner product $\langle (\Phi, \lambda, p), (\Phi', \lambda', p') \rangle_{\mathbb{H}} = \langle (\Phi, \Phi') \rangle_{H^1(\Omega^-)} + \langle (\lambda, \lambda'), H^{-\frac{1}{2}}(\Gamma_{\infty}) \rangle + \langle (p, p'), H^1(\Gamma_{\infty}) \rangle$.

If $f$ solves (35), then $(f^\perp, \gamma_1 f, 0)$ solves (43). Conversely, if $(\Phi, \lambda, p)$ solves (43), then $\mathcal{R}(\Phi, \lambda)$ solves (35) and $p = 0$, where $\mathcal{R}$ is defined in Section 4.3.

Theorem 4.4. Problem (43) is well-posed at all frequencies.

Proof. First, using Proposition 4.1, we can show that Problem (43) has at most one solution. Then, consider the two sesquilinear forms $a_1$ and $a_2$ on $\mathbb{H} \times \mathbb{H}$ such that

$$a_1((\Phi, \lambda, p), (\Phi', \lambda', p')) = \int_{\Omega} r \mathbf{v} \cdot \mathbf{v} \Phi' + \int_{\partial \Omega} N^0(\gamma_0^- \Phi), (\gamma_0^- \Phi') d\Gamma_{\infty} + \int_{\Omega} S^0(\lambda^0, \lambda') d\Omega_{\infty} + \delta_{\Gamma_{\infty}}(p, p')$$

and

$$a_2((\Phi, \lambda, p), (\Phi', \lambda', p')) = -\int_{\Omega} r k^2 \tilde{\partial} \Phi' + i \int_{\partial \Omega} r \mathbf{v} \cdot (\tilde{\partial} \Phi' - \Phi' \mathbf{v}) + \langle (N - N^0)(\gamma_0^- \Phi), (\gamma_0^- \Phi') \rangle_{\Gamma_{\infty}}$$

where $S^0, D^0, \tilde{D}^0$ and $N^0$ are the boundary integral operators $S, D, \tilde{D}$ and $N$ for $k_{\infty} = 0$. For the volumic term $\mathcal{V}$, our writing of the convected Helmholtz equation using the Prandtl–Glaucut transformation in the form (28a) allows us to readily see that $a_1$ is $\mathbb{H}$-coercive owing to (29). Then, since the linear map associated with $a_2$ is classically compact from $\mathbb{H}$ into $\mathbb{H}$ (see [41, Lemma 3.9.9]), the assertion follows by the Fredholm alternative and the uniqueness of the solution. \(\square\)

5. Finite-dimensional approximation

The coupled formulations (42) and (43) are approximated by FEM and BEM. We briefly recall the underlying results from both theories. Then, we discuss in more detail the structure of the linear systems and the algorithms for their numerical resolution.

5.1. Discrete finite element spaces

Let $\mathcal{M}$ be a shape-regular tetrahedral mesh of $\Omega^-$. The mesh $\mathcal{F}_{\infty}$ of $\Gamma_{\infty}$ is composed of the boundary faces of $\mathcal{M}$. Let $h_\mathcal{M} > 0$ denote the mesh size, $V^1_{\mathcal{M}}$ the space of continuous piecewise affine polynomials on $\mathcal{M}$, $S^0_{\mathcal{M}}$, the space of piecewise constant polynomials on $\mathcal{F}_{\infty}$, and $S^1_{\mathcal{M}}$, the space of continuous piecewise affine polynomials on $\mathcal{F}_{\infty}$. Let $\mathcal{H}_{\mathcal{M}} = V^1_{\mathcal{M}} \times S^0_{\mathcal{M}}$, and $\mathbb{H}_{\mathcal{M}} = V^1_{\mathcal{M}} \times S^0_{\mathcal{M}} \times S^1_{\mathcal{M}}$. The discretization of (42) reads: Find $(\Phi_{\mathcal{M}}, \lambda_{\mathcal{M}}) \in \mathbb{H}_{\mathcal{M}}$ such that, $\mathcal{V}(\Phi_{\mathcal{M}}', \lambda_{\mathcal{M}}', p_{\mathcal{M}}') \in \mathbb{H}_{\mathcal{M}}$,

$$a_{\text{unstab}}((\Phi_{\mathcal{M}}, \lambda_{\mathcal{M}}), (\Phi_{\mathcal{M}}', \lambda_{\mathcal{M}}')) = b_{\text{unstab}}(\Phi_{\mathcal{M}}', \lambda_{\mathcal{M}}'),$$

(45)
with $a_{\text{instab}}$ and $b_{\text{unstab}}$ readily deduced from (42), while the discretization of (43) reads: Find $(\Phi_M, \lambda_M, p_M) \in \mathcal{H}_M$ such that, $\forall (\Phi_{M}^i, \lambda_{M}^i, p_{M}^i) \in \mathcal{H}_M$:

$$a_{\text{stab}}((\Phi_M, \lambda_M, p_M), (\Phi_{M}^i, \lambda_{M}^i, p_{M}^i)) = b_{\text{stab}}((\Phi_{M}^i, \lambda_{M}^i, p_{M}^i)), \tag{46}$$

with $a_{\text{stab}}$ and $b_{\text{stab}}$ readily deduced from (43). Since $\mathcal{H}_M \subset \mathcal{H}$ and $\mathbb{H}_M \subset \mathbb{H}$, both approximations are conforming.

In what follows, $A \leq B$ denotes the inequality $A \leq cB$ with positive constant $c$ independent of the mesh size and of the discrete and exact solutions. Owing to classical approximation properties [7,15,41], there holds, $\forall (\Phi, \lambda) \in H^2(\Omega^-) \times H^\frac{1}{2}(\Gamma^-)$,

$$\inf_{(\Phi_{M}, \lambda_{M}, p_M) \in \mathcal{H}_M} \| (\Phi, \lambda) - (\Phi_{M}, \lambda_{M}) \| \lesssim h_M \left( \| \Phi \|_{H^2(\Omega^-)} + \| \lambda \|_{H^\frac{1}{2}(\Gamma^-)} \right), \tag{47}$$

and $\forall (\Phi, \lambda, p) \in H^2(\Omega^-) \times H^\frac{1}{2}(\Gamma^-) \times H^2(\Gamma^-)$,

$$\inf_{(\Phi_{M}, \lambda_{M}, p_M) \in \mathcal{H}_M} \| (\Phi, \lambda, p) - (\Phi_{M}, \lambda_{M}, p_M) \| \lesssim h_M \left( \| \Phi \|_{H^2(\Omega^-)} + \| \lambda \|_{H^\frac{1}{2}(\Gamma^-)} + \| p \|_{H^2(\Gamma^-)} \right). \tag{48}$$

**Remark 5.1.** Taking a polynomial approximation with one order less for $H^\frac{1}{2}(\Gamma^-)$ than for $H^1(\Omega^-)$ and $H^1(\Gamma^-)$ yields that all the approximations have the same order in $h_M$.

The following error estimates follow from [24, Theorem 13]: If $-\kappa^2 \notin A$ and $h_M$ is small enough, the discrete problem (45) has a unique solution $(\Phi_M, \lambda_M) \in \mathcal{H}_M$, and the following optimal error estimate holds:

$$\| (\Phi, \lambda) - (\Phi_M, \lambda_M) \| \lesssim \inf_{(\Phi_{M}^i, \lambda_{M}^i) \in \mathcal{H}_M} \| (\Phi, \lambda) - (\Phi_{M}^i, \lambda_{M}^i) \| \|, \tag{49}$$

where $(\Phi, \lambda)$ is the unique solution of (42). Moreover, at all frequencies and if $h_M$ is small enough, the discrete problem (46) has a unique solution $(\Phi_M, \lambda_M, p_M) \in \mathcal{H}_M$, and the following optimal error estimate holds:

$$\| (\Phi, \lambda, p) - (\Phi_M, \lambda_M, p_M) \| \lesssim \inf_{(\Phi_{M}^i, \lambda_{M}^i, p_{M}^i) \in \mathcal{H}_M} \| (\Phi, \lambda, p) - (\Phi_{M}^i, \lambda_{M}^i, p_{M}^i) \| \|, \tag{50}$$

where $(\Phi, \lambda, p)$ is the unique solution of (43).

**Remark 5.2.** The constant in (49) depends on $\kappa_M$, and its value explodes as $-\kappa^2$ tends to an element of $\Lambda$. The constant in (50) depends on $\kappa_M$ as well, but remains bounded on any bounded set of frequencies.

### 5.2. Structure of linear systems

#### 5.2.1. Unstable formulation with one surface unknown

Let $(\theta_i)_{1 \leq i \leq p}$ and $(\psi_i)_{1 \leq i \leq q}$ denote finite element bases for $V^1_{\mathcal{M}}$ and $S^0_{\mathcal{M}}$ respectively. These basis functions are real-valued. The decompositions of $\Phi_M \in V^1_{\mathcal{M}}$ and $\lambda_M \in S^0_{\mathcal{M}}$ on these bases are written in the form $\Phi_M = \sum_{i=1}^{p} \Phi_{M}^i \theta_i$ and $\lambda_M = \sum_{i=1}^{q} \lambda_{M}^i \psi_i$. Let

$$u_{\text{unstab}} = \begin{pmatrix} (\Phi_{M}^i)_{1 \leq i \leq p} \\ (\lambda_{M}^i)_{1 \leq i \leq q} \end{pmatrix}, \quad b_{\text{unstab}} = \begin{pmatrix} (\gamma_1 f_{\text{inc}}, \gamma_0^i \theta_i)_{\Gamma_i} \\ (-\gamma_0 f_{\text{inc}}, \gamma_0^i \theta_i)_{\Gamma_i} \end{pmatrix},$$

$$A_{\text{unstab}} = \begin{pmatrix} (\nabla (\theta_j, \theta_i) + (N(\gamma_0^i \theta_j), \gamma_0^i \theta_i)_{\Gamma_i} & ((\tilde{D} - \frac{1}{2}I)(\psi_j), \gamma_0^i \theta_i)_{\Gamma_i} \\ (-\nabla (\theta_j, \psi_i) - (N(\gamma_0^i \theta_j), \psi_i)_{\Gamma_i} & (-S(\psi_j), \psi_i)_{\Gamma_i} \end{pmatrix}, \tag{52}$$

where in $A_{\text{unstab}}$ the index $i$ refers to the rows and the index $j$ to the columns. The linear system resulting from (45) is

$$A_{\text{unstab}} u_{\text{unstab}} = b_{\text{unstab}}. \tag{53}$$

To better understand the structure of the linear system (53), the basis functions $(\theta_i)_{1 \leq i \leq p}$ of $V^1_{\mathcal{M}}$ are separated into two sets: the basis functions $(\theta_i^M)_{1 \leq i \leq p \wedge F}$ associated with the mesh vertices located in $F$, and $(\theta_i^M)_{1 \leq i \leq p \wedge S}$ associated with the mesh vertices located in $S$; clearly, $p = p^F + p^S$. The matrix $A_{\text{unstab}}$ can then be further decomposed as

$$A_{\text{unstab}} = \begin{pmatrix} A_{\text{instab}} & A_{\text{stab}} & 0 \\ A_{\text{instab}}^T & A_{\text{instab}}^T & A_{\text{instab}}^T \\ 0 & A_{\text{instab}}^T & A_{\text{instab}}^T \end{pmatrix}, \tag{54}$$
where \((A^{\text{stab}}_{1,1})_{i,j} = \mathcal{V}(\theta_j^{\text{stab}}, \theta_i^{\text{stab}}), (A^{\text{stab}}_{1,2})_{i,j} = \mathcal{V}(\theta_j^{\text{stab}}, \theta_i^{\text{stab}}), (A^{\text{stab}}_{2,1})_{i,j} = \mathcal{V}(\theta_j^{\text{stab}}, \theta_i^{\text{stab}}), (A^{\text{stab}}_{2,2})_{i,j} = \mathcal{V}(\theta_j^{\text{stab}}, \theta_i^{\text{stab}}) + (N(Y_0 \theta_j^{\text{stab}} \psi_j, Y_0 \theta_i^{\text{stab}} \psi_i) r_{\infty}, (A^{\text{stab}}_{2,3})_{i,j} = ((\bar{D} - \frac{1}{2} I) (\psi_j), (Y_0 \theta_i^{\text{stab}} \psi_i) r_{\infty} , (A^{\text{stab}}_{3,2})_{i,j} = ((\bar{D} - \frac{1}{2} I) (\psi_j), (\psi_i) r_{\infty} , (A^{\text{stab}}_{3,3})_{i,j} = ((\bar{D} - \frac{1}{2} I) (\psi_j), (\xi_i) r_{\infty} , (A^{\text{stab}}_{3,4})_{i,j} = -(\mathcal{S}(\psi_j), (\psi_i) r_{\infty} , (A^{\text{stab}}_{4,2})_{i,j} = -((\bar{D} - \frac{1}{2} I) (\psi_j), (\xi_i) r_{\infty} , (A^{\text{stab}}_{4,3})_{i,j} = -((\bar{D} - \frac{1}{2} I) (\psi_j), (\xi_i) r_{\infty} , (A^{\text{stab}}_{4,4})_{i,j} = -((\bar{D} - \frac{1}{2} I) (\psi_j), (\xi_i) r_{\infty}.

All the blocks are complex-valued. The blocks \(A_{1,1}^{\text{stab}}\) and \(A_{2,2}^{\text{stab}}\) are sparse. The block \(A_{1,2}^{\text{stab}}\) is not symmetric, and the block \(A_{1,2}^{\text{stab}}\) is neither the transpose nor the Hermitian transpose of the block \(A_{2,1}^{\text{stab}}\). The block \(A_{2,2}^{\text{stab}}\) has two contributions: one sparse and non-symmetric and one dense and symmetric; therefore, this block is dense and non-symmetric. The blocks \(A_{2,3}^{\text{stab}}, A_{3,2}^{\text{stab}}\) and \(A_{3,3}^{\text{stab}}\) are dense. The block \(A_{3,3}^{\text{stab}}\) is the transpose of the block \(A_{3,3}^{\text{stab}}\), and the block \(A_{3,3}^{\text{stab}}\) is symmetric.

5.2.2. Stable formulation with two surface unknowns

Let \((\xi_1)_{1 \leq i \leq p}\) denote a finite element basis for \(S^1\). The decomposition of \(p_M \in S^1\) on this basis is written in the form

\[
p_M = \sum_{i=1}^p p_M^i \xi_i.
\]

Let \(u_M^{\text{stab}} = (\Phi_{M1})_{1 \leq i \leq p}, (\lambda_{M1})_{1 \leq i \leq q}, (\rho_{M1})_{1 \leq i \leq r} \) and \(B^{\text{stab}} = ((\gamma_I)_{1 \leq i \leq p}, (\gamma_I)_{1 \leq i \leq q}, (\gamma_I)_{1 \leq i \leq r} \).

\[\begin{pmatrix}
\mathcal{V}(\theta_j, \theta_i) + (N(Y_0 \theta_j) Y_0 \theta_i) r_{\infty} \\
((\bar{D} - \frac{1}{2} I) (\psi_j), (\psi_i) r_{\infty} \\
((\bar{D} - \frac{1}{2} I) (\psi_j), (\xi_i) r_{\infty} \\
(\mathcal{S}(\psi_j), (\psi_i) r_{\infty} \\
(\mathcal{S}(\psi_j), (\xi_i) r_{\infty) \\
(\mathcal{S}(\psi_j), (\xi_i) r_{\infty) \\
(\mathcal{S}(\psi_j), (\xi_i) r_{\infty) \\
(\mathcal{S}(\psi_j), (\xi_i) r_{\infty)
\end{pmatrix} = 0,
\]

with the same convention as above on the indices \(i\) and \(j\) of \(A^{\text{stab}}\). The linear system resulting from (46) is

\[
A^{\text{stab}} u_M^{\text{stab}} = B^{\text{stab}}.
\]

As in the previous section, the matrix of the linear system (57) is further decomposed as

\[
A^{\text{stab}} = \begin{pmatrix}
A_{1,1}^{\text{stab}} & A_{1,2}^{\text{stab}} & 0 & 0 \\
A_{2,1}^{\text{stab}} & A_{2,2}^{\text{stab}} & A_{2,3}^{\text{stab}} & 0 \\
0 & A_{3,2}^{\text{stab}} & A_{3,3}^{\text{stab}} & A_{3,4}^{\text{stab}} \\
0 & A_{4,2}^{\text{stab}} & A_{4,3}^{\text{stab}} & A_{4,4}^{\text{stab}}
\end{pmatrix}.
\]

5.3. Numerical resolution

Both the unstable and stable formulations have been implemented in the EADS in-house boundary element software called ACTIPOLE. This software can treat general three-dimensional geometries. The iterative solver is a GMRES solver [40] with no restart, suitable for non-symmetric linear systems (an additional feature of the solver is that it can treat multiple right-hand sides [27,37]). The specificity of each block in (54) or (58) is taken into account. Matrix-vector products involving sparse blocks are optimized accordingly, and those involving dense blocks resulting from boundary integral terms can be accelerated using a fast multipole method and out-of-core parallelization techniques.

The preconditioner uses a combination of a sparse approximate inverse (SPAI) preconditioner [9,10] and the sparse direct solver MUMPS [1]. More precisely, for the dense diagonal blocks \(A_{2,2}^{\text{stab}}, A_{3,3}^{\text{stab}}\) and \(A_{4,4}^{\text{stab}}\), the SPAI preconditioner searches for an approximation of the inverse of these blocks. Letting \(A\) denote any of these blocks, \(A\) is made sparse by keeping, in each column, the interaction terms between the corresponding basis function and the ones in its vicinity (in the sense of vertices or faces). The result of this operation is denoted by \(A^p\), and we define the set of matrices having the same sparsity pattern, i.e., \(S^A = \{M \in \mathbb{C}^{p,n} | M_{i,j} = 0 \forall 1 \leq i, j \leq n \text{ s.t. } A^p_{i,j} = 0\}\) where \(n\) is the number of rows of \(A\). The SPAI preconditioner of \(A\) is then given by \(P = \arg \min_{M \in S^A} \|A^p M - I\|_F\), where \(\| \cdot \|_F\) denotes the Frobenius norm. For the blocks \(A_{2,2}^{\text{stab}}\) and \(A_{4,4}^{\text{stab}}\), the SPAI preconditioner is computed ignoring the volumetric contributions. For the sparse diagonal blocks, the preconditioner is taken as the inverse of each block. The inverse is not actually computed: since MUMPS provides a factorization of each of these blocks, each time a preconditioner-vector product is needed when constructing the Krylov vectors of the iterative method, two triangular systems are efficiently solved using this factorization. The preconditioner for the whole system is block diagonal, each block being a SPAI or MUMPS preconditioner.
Table 1
Characteristics of the four considered meshes.

<table>
<thead>
<tr>
<th></th>
<th>Mesh 1</th>
<th>Mesh 2</th>
<th>Mesh 3</th>
<th>Mesh 4</th>
</tr>
</thead>
<tbody>
<tr>
<td>Number of volumic dofs $\Phi$</td>
<td>1796</td>
<td>687</td>
<td>194</td>
<td>79</td>
</tr>
<tr>
<td>Number of surfacic $P_0$ dofs $\lambda$</td>
<td>808</td>
<td>510</td>
<td>270</td>
<td>148</td>
</tr>
<tr>
<td>Number of surfacic $P_1$ dofs $p$</td>
<td>406</td>
<td>257</td>
<td>137</td>
<td>76</td>
</tr>
<tr>
<td>Proportion of dofs $p$ in the total number of dofs</td>
<td>11.9%</td>
<td>15.0%</td>
<td>18.6%</td>
<td>20.0%</td>
</tr>
<tr>
<td>Smallest edge (mm)</td>
<td>7.09</td>
<td>8.78</td>
<td>15.71</td>
<td>19.18</td>
</tr>
<tr>
<td>Mean edge (mm)</td>
<td>22.64</td>
<td>32.20</td>
<td>49.78</td>
<td>66.46</td>
</tr>
<tr>
<td>Largest edge (mm)</td>
<td>56.87</td>
<td>70.62</td>
<td>103.59</td>
<td>112.71</td>
</tr>
</tbody>
</table>

Fig. 3. Left: representation of Mesh 1, right: potential flow around the ellipsoid.

6. Numerical results

The purpose of this section is the comparison between the unstable formulation (42) and the stable formulation (43) with the coupling parameter $\eta = 1$.

Consider an ellipsoid with major axis directed along the $z$-axis. This object is included inside a larger ball. The external border of the ball after discretization is the surface $\Gamma_\infty$. A potential flow is computed around the ellipsoid and inside the ball, such that the flow is uniform outside the ball, of Mach number 0.3 and directed along the $z$-axis. An acoustic monopole source lies upstream of the ball, on the $z$-axis as well. Four different meshes are considered, see Table 1. For accuracy reasons, a rule of thumb in boundary element methods for the classical Helmholtz equation is to set the mean edge length to a value eight to ten times smaller than the wavelength of the source. In our simulations, we first generate the mesh and then apply the Prandtl–Glauert transformation. With the present choice for the Mach number, the mesh is at most extended by a factor $\gamma_\infty \approx 1.048$. Moreover, the integral operators are computed at the transformed wavenumber $\hat{k}_\infty = \gamma_\infty k_\infty \approx 0.21$ m. We then verify that, for Mesh 1, the mean length of the edges of the transformed mesh is eight times smaller than the wavelength. The three coarser meshes do not satisfy the rule of thumb and are used as comparison supports and in numerical experiments requiring a large number of resolutions.

From Table 1, for fine meshes, the number of basis functions used to discretize the unknown $p$ in the variational formulation (43) takes a smaller part in the total number of basis functions than for coarse meshes (from 20% down to 12%). Therefore, the relative complexity added to (42) by the third equation of (43) decreases with the total number of unknowns, which is an interesting property when it comes to industrial test cases. Fig. 3 displays Mesh 1 and the rescaled velocity $M_0$ of the potential flow.

In what follows, a frequency $\nu$ is called resonant if $-\frac{\hat{k}^2_\infty}{\gamma_\infty^2} = -\frac{4\pi^2 \nu^2}{\gamma_\infty^2} \in \Lambda$, where $\Lambda$ is the set of Dirichlet eigenvalues for the Laplacian on $\mathbb{R}^3 \setminus \overline{\Omega^\nu}$. The set $\Lambda$ depends on the shape of the coupling surface $\Gamma_\infty$, which slightly changes after each discretization.
6.1. Comparison of pressure fields

As seen in Theorem 4.2, the unstable formulation (42) is not well-posed at resonant frequencies. First, a prospective study to identify a resonant frequency for each of the four meshes is carried out by monitoring the condition number of the corresponding matrices. A resonant frequency for Mesh 1, Mesh 2, Mesh 3, and Mesh 4 is identified around 1509.849 Hz, 1513.431 Hz, 1521.015 Hz, and 1535.704 Hz, respectively.

The convergence of the iterative solver is monitored by requiring that the Euclidean norm of the relative residual is smaller than $10^{-6}$. Additional tests indicate that the discretized solution to the stable formulation does not change much below this value of the relative residual. For Mesh 1, away from a resonance, say at 1500 Hz, the scattered pressure fields computed with the unstable and stable formulations are very similar. This holds as well for the total pressure fields, see Fig. 4. At the resonant frequency 1509.849 Hz, the unstable formulation (42) yields pressure maps quite different from the ones at 1500 Hz, whereas the stable formulation (43) yields pressure maps very similar to the ones at 1500 Hz, see Fig. 5. The distortion of the scattered field with the unstable formulation (42) is the result of the significant magnification of numerical errors by the ill-conditioning of the linear system approximating (42).

6.2. Auxiliary variable $p$

In Fig. 6, the left plot indicates that with Mesh 1, the magnitude of $p$ is around 0.5% of the scattered pressure. The right plot shows the behavior of the magnitude of $p$ (measured as $\|p\|_{L^\infty(\Gamma_\infty)}$) with respect to the stopping criterion of the iterative solver for the four meshes. The finer the mesh, the smaller the auxiliary variable $p$, which is consistent with the fact that the $p$-component of the solution to (43) vanishes (see Section 4.4).
Fig. 5. Mesh 1, 1500.849 Hz. Top: real part of the total pressure; left: unstable formulation (42), right: stable formulation (43). Bottom: real part of the scattered pressure; left: unstable formulation (42), right: stable formulation (43). At this resonant frequency, the two formulations yield different results.

Fig. 6. Stable formulation (43) at 1500 Hz. Left: real part of the scattered pressure and auxiliary variable \( p \) with Mesh 1. Right: magnitude of the auxiliary variable \( p \) as a function of the stopping criterion of the iterative linear solver with all meshes.

6.3. Comparison of condition numbers

Fig. 7 presents the condition numbers of the matrices resulting from the formulations (42) and (43) as a function of the frequency. In the left plot, the curves are centered at the resonant frequencies. The finer the mesh, the higher the condition number explodes. The width of the peak at the resonance does not appear to depend on the mesh. In the right plot, a larger frequency bandwidth is considered with Mesh 2. Owing to the frequency sampling (every 5 Hz), some resonances may be
missed, and the local maxima may not be accurately reached (in particular, from the left plot, the local maximum of 7.2 for \( \log(\text{cond}(M)) \) at 1513.431 Hz is very underestimated). The stable formulation (43) produces somewhat larger condition numbers for the large majority of the frequencies, but, unlike the unstable formulation (42), it presents no resonance. Moreover, from the Weyl formula, the number of resonant frequencies smaller than \( f \) increases as \( f^2 \), making the need for a stable formulation even more important for simulations at higher frequencies.

6.4. Convergence

To further study the impact of the ill-conditioning of the unstable formulation (42) on the computed solution, the preconditioning is not used in what follows. First, the value of the acoustic pressure on a network of 10,000 points located further than 0.5 m from the center of the sphere (therefore in \( \Omega^+ \)) is computed using the stable formulation (43) with Mesh 1 at the resonant frequency 1509.849 Hz. This computed acoustic pressure is called the accurate pressure. Next, the acoustic pressure on the same network of points is computed for different values of the number of iterations of the solver, using the unstable formulation (42) and the stable formulation (43) with Mesh 1 at the same frequency. The relative difference between the computed pressure and the accurate pressure in Euclidean norm is called the relative error. Fig. 8 presents the relative residual and the relative error with respect to the number of iterations. With the unstable formulation (42), the relative residual decreases irregularly. In particular, it stays constant during around 200 iterations. The relative error decreases, stays constant, rises after 400 iterations, and finally stabilizes at a large value, whereas the relative residual keeps converging to zero. As for every ill-conditioned problem, the relative residual cannot be used to ascertain convergence towards the correct solution. In particular, after 600 iterations, the relative residual is extremely small, while the error is of order one. With the stable formulation (43), the relative residual and the relative error decrease regularly, and in the same fashion.
Fig. 9. Condition number of the matrix for the stable formulation (43) centered around the resonant frequency at 1535.704 Hz for Mesh 4. In this case, the chosen value $\eta = 1$ leads to the minimal condition numbers.

6.5. Choice of the coupling parameter $\eta$

In the stable formulation (43), the choice of the coupling parameter $\eta$ is expected to have a direct effect of the condition number of the matrix $A_{\text{stab}}$. In Fig. 9, this condition number is plotted for Mesh 4 and for various values of $\eta$. For $\eta = 0$, Eqs. (43a)–(43b) are decoupled from (43c), and (43a)–(43b) become (42), so that the curve for $\eta = 0.001$ is similar to the curve of the unstable formulation for Mesh 4 in Fig. 7. The condition number appears to be the smallest for $\eta$ in the range 1 to 10, and worsens for lower and higher values of $\eta$. This motivates the choice $\eta = 1$ made in the above simulations.

7. Conclusion

In this work, we derived two coupled formulations for the convected Helmholtz equation with non-uniform flow in a bounded domain. The first formulation involves one surface unknown and is well-posed except at some resonant frequencies of the source, while the second formulation is unconditionally well-posed and involves two surface unknowns. Our numerical results show that at resonant frequencies, the discretization of the first formulation is ill-conditioned so that the pressure field is plagued by spurious oscillations. Moreover, the second formulation remains tractable within large industrial problems since the relative complexity added by the second surface unknown decreases with the size of the mesh. The interest in the second formulation is also enhanced by the fact that, at higher frequencies, the density of resonant frequencies is more important.

As long as the uniform flow assumption in the exterior domain is reasonable, more complex flows in the interior domain can be considered, as well as more complex boundary conditions at the surface of the scattering object. These extensions only require to modify the finite element part of the present methodology.

Another interesting extension of this work is the resolution of parametrized aeroacoustic problems, with the frequency of the source as a parameter, using reduced-order models, for instance by means of Proper Generalized Decomposition or Reduced Basis methods. Using the first formulation may involve ill-conditioned numerical resolutions if the frequency range of interest contains resonant frequencies, whereas the second formulation guarantees well-posedness of the procedure. Moreover, the complexity of the online stage of the reduced-order model is not increased when using the second formulation.

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